



When Recorded Mail To:  
American Fork City  
51 East Main  
American Fork UT 84003

ENT 24373:2020 PG 1 of 50  
JEFFERY SMITH  
UTAH COUNTY RECORDER  
2020 Feb 26 11:18 am FEE 40.00 BY SW  
RECORDED FOR AMERICAN FORK CITY

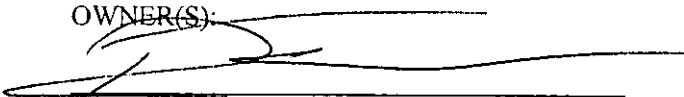
NOTICE OF INTEREST, BUILDING REQUIREMENTS, AND  
ESTABLISHMENT OF RESTRICTIVE COVENANTS

This Notice is recorded to bind the attached Geotechnical Study dated January 11, 2017 along with the site grading plan to the property generally located at 700 South 290 West, American Fork, UT 84003 and therefore mandating that all construction be in compliance with said Geotechnical Study and site grading plan per the requirements of American Fork City ordinances and standards and specification including specifically Ordinance 07-10-47, Section 6-5, Restrictive Covenant Required and 6-2-4, Liquefiable Soils. Said Sections require establishment of a restrictive covenant and notice to property owners of liquefiable soils or other unique soil conditions and construction methods associated with the property.

- Exhibit A – Legal Description of Property
- Exhibit B – Geotechnical Study
- Exhibit C – Site Grading Plan

Dated this 21<sup>st</sup> day of February 2020.

OWNER(S):

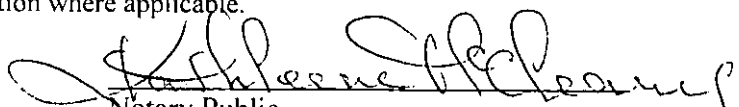
  
(Signature)

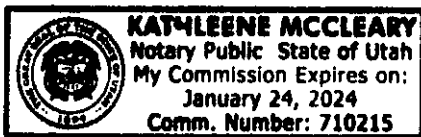
Robert Thomson  
(Printed Name)

Manager  
(Title)

STATE OF UTAH                    )  
  §  
COUNTY OF \_\_\_\_\_)

On the 21<sup>st</sup> day of February, 2020, personally appeared before me, Robert Thomson, Owner(s) of said Property, as (individuals and/or authorized representatives of a company), and acknowledged to me that such individuals or company executed the within instrument freely of their own volition and pursuant to the articles of organization where applicable.

  
Notary Public  
My Commission Expires: 1-24-2024



## Exhibit A

Parcel Number: 13:065:0066

Legal Description: COM AT SW COR. SEC. 23, T5S, R1E, SLB&M.; N 0 DEG 3' 42" E 93.4 FT; S 88 DEG 53' 7" E 499.08 FT; N 5 DEG 54' 46" E 35.62 FT; N 81 DEG 54' 36" E 697.45 FT; S 29.76 FT; S 88 DEG 22' 0" E 511.11 FT; S 1 DEG 2' 0" W 466.97 FT; S 0 DEG 52' 0" W 552 FT; S 89 DEG 57' 0" W 197.23 FT; N 88 DEG 39' 0" W 110 FT; S 89 DEG 50' 0" W 96 FT; N 88 DEG 45' 0" W 52.75 FT; S 88 DEG 43' 0" W 123.5 FT; N 88 DEG 30' 0" W 113.5 FT; N 18 DEG 0' 0" E 3.17 FT; N 89 DEG 29' 0" W 702.48 FT; N 0 DEG 28' 0" E 306.31 FT; W 294.57 FT; N 0 DEG 6' 15" W 526.75 FT TO BEG. AREA 36.332 AC.

Parcel Number: 13:065:0066

Legal Description: COM E 1193.24 FT & N 187.5 FT FR SW COR. SEC. 23, T5S, R1E, SLB&M.; N 36.14 FT; S 88 DEG 35' 0" E 512.6 FT; S 38.08 FT; N 88 DEG 22' 0" W 512.66 FT TO BEG. AREA 0.436 AC.



1497 West 40 South  
Lindon, Utah - 84042  
Phone (801) 225-5711

3662 West 2100 South  
Salt Lake City, Utah - 84120  
Phone (801) 787-9138

1596 W. 2650 S. #108  
Ogden, Utah - 84401  
Phone (801) 399-9516

**Geotechnical Study  
American Fork Property  
700 South 400 West  
American Fork, Utah**

**Project No. 169273**

January 11, 2017

*Prepared For:*

Woodside Homes  
Attention: Mr. Garrett Seely  
460 West 50 North, Suite 200  
Salt Lake City, UT 84101

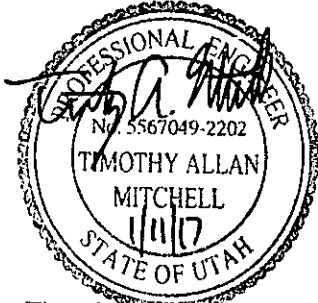
*Prepared By:*

**EARTHTEC ENGINEERING**  
Lindon Office



### CERTIFICATE

I hereby certify that I am a licensed professional engineer, as defined in the "Sensitive Lands Ordinance" Section of American Fork City Ordinances. I have examined this report to which this certificate is attached and the information and conclusions contained therein are, without any reasonable reservation not stated therein, accurate and complete. All procedures and tests used in this report meet minimum applicable professional standards.



Timothy A. Mitchell, P.E.  
Geotechnical Engineer



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**ATTACHED FIGURES**

No. 1 VICINITY MAP  
 No. 2 AERIAL PHOTOGRAPH SHOWING LOCATION OF BORING AND TEST PITS  
 Nos. 3 – 11 BORING AND TEST PIT LOGS  
 No. 12 LEGEND  
 Nos. 13 – 19 CONSOLIDATION-SWELL TEST



## 1.0 EXECUTIVE SUMMARY

This entire report presents the results of Earthtec Engineering's completed geotechnical study for the American Fork Property in American Fork, Utah. This executive summary provides a general synopsis of our recommendations and findings. Details of our findings, conclusions, and recommendations are provided within the body of this report.

- The subject property is approximately 48 acres and is proposed to be developed with the construction of a subdivision consisting of single-family residences. The proposed structures will consist of conventionally framed, two- to three-story, buildings with the possibility of basements. We anticipate foundation loads for the proposed structures will not exceed 5,000 pounds per linear foot for bearing wall, 30,000 pounds for column loads, and 100 pounds per square foot for floor slabs. (see Section 3)
- Our field exploration included the boring of one (1) boring and the excavation of eight (8) test pits to depth of 9½ to 71½ feet below the existing ground surface. Groundwater was encountered at depths of approximately 6 to 9 feet below the existing ground surface. (see Section 5)
- The native sand, clay and silt soils have a slight to moderate potential for collapse (settlement) and a high potential for compressibility under increased moisture contents and anticipated load conditions. (see Section 6)
- The subsurface soils encountered generally consisted of topsoil overlying soft to stiff clay and silt, and very loose to dense sand and gravel. All topsoil should be removed beneath the entire building footprints, exterior flatwork, and pavements prior to construction. (see Section 7)
- The silt and sand layers between depths of 13 to 25 feet have a "High" potential for liquefaction during a moderate to large earthquake event; should this layer liquefy, we estimate that up to 3½ inches of liquefaction-induced settlement and up to 2½ feet of liquefaction-induced lateral movements could occur. (see Section 9)
- Conventional strip and spread footings may be used to support the structure, with foundations placed entirely on a minimum of 24 inches of undisturbed gravel soils or on a minimum 18 inches of properly placed, compacted, and tested structural fill extending to undisturbed native soils. (see Section 10)
- Minimum roadway section consists of 3 inches of asphalt and 12 inches of road-base. Areas that are soft or deflect under construction traffic should be removed and replaced with granular material or structural fill. (see Section 13)

Based on the results of our field exploration, laboratory testing, and engineering analyses, it is our opinion that the subject site may be suitable for the proposed development, provided the recommendations presented in this report are followed and implemented during design and



construction.

Failure to consult with Earthtec Engineering (Earthtec) regarding any changes made during design and/or construction of the project from those discussed herein relieves Earthtec from any liability arising from changed conditions at the site. We also strongly recommend that Earthtec observes the building excavations to verify the adequacy of our recommendations presented herein, and that Earthtec performs materials testing and special inspections for this project to provide continuity during construction.

## 2.0 INTRODUCTION

The project is located at approximately 700 South 400 West in American Fork, Utah. The general location of the site is shown on Figure No. 1, *Vicinity Map* and Figure No. 2, *Aerial Photograph Showing Location of Boring and Test Pits*, at the end of this report. The purposes of this study are to:

- Evaluate the subsurface soil conditions at the site,
- Assess the engineering characteristics of the subsurface soils, and
- Provide geotechnical recommendations for general site grading and the design and construction of foundations, concrete floor slabs, miscellaneous concrete flatwork, and asphalt paved residential streets.

The scope of work completed for this study included field reconnaissance, subsurface exploration, field and laboratory soil testing, geotechnical engineering analysis, and the preparation of this report.

## 3.0 PROPOSED CONSTRUCTION

We understand that the proposed project, as described to us by Mr. Garrett Seely with Woodside Homes, consists of developing the approximately 48-acre existing parcel with the construction of a subdivision consisting of single-family residences. The proposed structures will consist of conventionally framed, two- to three-story, buildings with the possibility of basements. We have based our recommendations in this report on the assumption that or anticipated foundation loads for the proposed structures will not exceed 5,000 pounds per linear foot for bearing wall, 30,000 pounds for column loads, and 100 pounds per square foot for floor slabs. If structural loads will be greater Earthtec should be notified so that we may review our recommendations and make modifications, if necessary.

In addition to the construction described above, we anticipate that

- Utilities will be installed to service the proposed buildings,
- Exterior concrete flatwork will be placed in the form of curb, gutter, and sidewalks, and





- Asphalt paved residential streets will be constructed.

## 4.0 GENERAL SITE DESCRIPTION

### 4.1 Site Description

At the time of our subsurface exploration the site was an undeveloped alfalfa field. The ground surface appears to be relatively flat, we anticipate less than 3 feet of cut and fill may be required for site grading. The lot was bounded on the north, south and west by undeveloped fields, and on the east by Storrs Avenue.

### 4.2 Geologic Setting

The subject property is located in the central portion of Utah Valley near the northeastern shore of Utah Lake. Utah Valley is a deep, sediment-filled basin that is part of the Basin and Range Physiographic Province. The valley was formed by extensional tectonic processes during the Tertiary and Quaternary geologic time periods. The valley is bordered by the Wasatch Mountain Range on the east and the Lake Mountains on the west. Much of northwestern Utah, including Utah Valley, was previously covered by the Pleistocene age Lake Bonneville. Utah Lake, which currently covers much of the western portion of the valley, is a remnant of this ancient fresh water lake. The surficial geology of much of the eastern margin of the valley has been mapped by Constenius, 2011<sup>1</sup>. The surficial geology at the location of the subject site and adjacent properties is mapped as:

- "Fine-grained lacustrine deposits" (Map Unit Qlf) dated to be upper Pleistocene. These soil or deposits are generally described in the referenced mapping as "silt and clay with some finegrained sand."
- "Younger alluvial-fan deposits" (Map Unit Qafy) dated to be Holocene and upper Pleistocene. These soil or deposits are generally described in the referenced mapping as "sand, silt and gravel."

## 5.0 SUBSURFACE EXPLORATION

### 5.1 Soil Exploration

Under the direction of a qualified member of our geotechnical staff, subsurface explorations were conducted at the site on December 20, 2016 by the boring of one (1) boring and the excavation of eight (8) test pits to depth of 9½ to 71½ feet below the existing ground surface using a a truck-mounted hydraulic drill rig and a track-mounted mini excavator. The approximate locations of the test pits are shown on Figure No. 2, *Aerial Photograph Showing*

<sup>1</sup> Constenius, K.N., Clark, D.L., King, J.K., Ehler, J.B., 2011, Interim Geologic Map of the Provo Quadrangle, *Utah, Wasatch and Salt Lake Counties, Utah*; U.S. Geological Survey, Open-File 586DM, Scale 1: 62,500.



*Location of Boring and Test Pits.* Graphical representations and detailed descriptions of the soils encountered are shown on Figure Nos. 3 through 11, *Boring and Test Pit Log* at the end of this report. The stratification lines shown on the logs represent the approximate boundary between soil units; the actual transition may be gradual. Due to potential natural variations inherent in soil deposits, care should be taken in interpolating between and extrapolating beyond exploration points. A key to the symbols and terms on the logs is presented on Figure No. 12, *Legend*.

Samples of the subsurface soils were collected in the borings at depth intervals of approximately 2½ to 5 feet. Relatively undisturbed samples were collected by pushing thin-walled "Shelby" tubes into undisturbed soils below the augers. Disturbed samples were collected with a 1¾ inch inside diameter split spoon sampler. The split spoon sampler was driven 18 inches into undisturbed soil with a 140-pound hammer free-falling through a distance of 30 inches. The blows required to drive the sampler through the final 12 inches of penetration is called the "N-value" or "blow count," and is recorded as "blows per foot" on the attached boring logs at the respective sample depths. The blow count provides a reasonable indication of the in-place relative density of sandy soils, but provides only a limited indication of the relative stiffness of cohesive (clayey) materials, since the penetration resistance for these soils is a function of the moisture content. In gravelly soils, the blow count may be higher than it otherwise would be, particularly when one or more gravel particles are larger than the sampler diameter. Disturbed bag samples and relatively undisturbed block samples were collected at various depths in each test pit.

The soil samples collected were classified by visual examination in the field following the guidelines of the Unified Soil Classification System (USCS). The samples were transported to our Lindon, Utah laboratory where they will be retained for 30 days following the date of this report and then discarded, unless a written request for additional holding time is received prior to the 30-day limit.

## 6.0 LABORATORY TESTING

Representative soil samples collected during our field exploration were tested in the laboratory to assess pertinent engineering properties and to aid in refining field classifications, if needed. Tests performed included natural moisture content, dry density tests, liquid and plastic limits determinations, mechanical (partial) gradation analyses, and one-dimensional consolidation tests. The table below summarizes the laboratory test results, which are also included on the attached *Boring and Test Pit Logs* at the respective sample depths, and on Figure Nos. 13 through 19, *Consolidation-Swell Test*.



**Table 1: Laboratory Test Results**

Boring and Test Pit No.	Depth (ft.)	Natural Moisture (%)	Natural Dry Density (pcf)	Atterberg Limits		Grain Size Distribution (%)			Soil Type
				Liquid Limit	Plasticity Index	Gravel (+ #4)	Sand	Silt/Clay (- #200)	
B-1	5	24	---	31	10	23	41	36	SC
B-1	15	---	---	44	14	---	---	---	SM
B-1	20	21	---	---	---	33	54	13	SM
B-1	40	33	---	39	18	0	23	77	CL
TP-1	5	40	65	35	4	4	52	44	SM
TP-2	5½	25	---	25	4	3	44	53	CL-ML
TP-2	6½	21	87	32	12	14	21	65	CL
TP-3	4	34	71	50	24	8	44	48	CH
TP-4	8	25	94	28	10	8	32	60	CL
TP-6	4	28	86	29	7	7	24	69	CL-ML
TP-7	8	68	51	41	9	22	24	54	ML
TP-8	2½	18	65	39	8	11	31	58	ML

NP\* = Non-Plastic

As part of the consolidation test procedure, water was added to the samples to assess moisture sensitivity when the samples were loaded to an equivalent pressure of approximately 1,000 psf. The native sand, clay and silt soils have a slight to moderate potential for collapse (settlement) and a high potential for compressibility under increased moisture contents and anticipated load conditions.

## 7.0 SUBSURFACE CONDITIONS

### 7.1 Soil Types

On the surface of the site, we encountered topsoil which is estimated to extend up to 2 feet in depth at the boring and test pit locations. Below the topsoil we encountered layers of clay, silt, sand, and gravel extending to depth of 9½ to 71½ feet below the existing ground surface. Graphical representations and detailed descriptions of the soils encountered are shown on Figure Nos. 3 through 11, *Boring and Test Pit Log* at the end of this report. Based on the blow counts obtained and our experience and observations during field exploration, the clay and silt soils ranged from soft to stiff in consistency and the sand and gravel soils had a relative density varying from very loose to dense.

Topsoil material composition and contacts are difficult to determine from boring sampling. Variation in topsoil depths may occur at the site.



## **7.2 Groundwater Conditions**

Groundwater was encountered at depths of approximately 6 to 9 feet below the existing ground surface. Note that groundwater levels will fluctuate in response to the season, precipitation, snow melt, irrigation, and other on and off-site influences. Quantifying these fluctuations would require long term monitoring, which is beyond the scope of this study. The contractor should be prepared to dewater excavations as needed.

## **8.0 SITE GRADING**

### **8.1 General Site Grading**

All surface vegetation and unsuitable soils (such as topsoil, organic soils, undocumented fill, soft, loose, or disturbed native soils, and any other inapt materials) should be removed from below foundations, floor slabs, exterior concrete flatwork, and pavement areas. We encountered topsoil on the surface of the site. The topsoil (including soil with roots larger than about ¼ inch in diameter) should be completely removed, even if found to extend deeper, along with any other unsuitable soils that may be encountered. Over-excavations below footings and slabs also may be needed, as discussed in Section 10.0.

Fill placed over large areas, even if only a few feet in depth, can cause consolidation in the underlying native soils resulting in settlement of the fill. Because the site is relatively flat, we anticipate that less than 3 feet of grading fill will be placed. If more than 3 feet of grading fill will be placed above the existing surface (to raise site grades), Earthtec should be notified so that we may provide additional recommendations, if required. Such recommendations will likely include placing the fill several weeks (or possibly more) prior to construction to allow settlement to occur.

### **8.2 Temporary Excavations**

Temporary excavations that are less than 4 feet in depth and above groundwater should have side slopes no steeper than ½H:1V (Horizontal:Vertical). Temporary excavations where water is encountered in the upper 4 feet or that extend deeper than 4 feet below site grades should be sloped or braced in accordance with OSHA<sup>2</sup> requirements for Type C soils.

### **8.3 Fill Material Composition**

The native soils are not suitable for use as placed and compacted structural fill. Excavated soils, including clay and silt, may be stockpiled for use as fill in landscape areas.

Structural fill is defined as fill material that will ultimately be subjected to any kind of structural loading, such as those imposed by footings, floor slabs, pavements, etc. We recommend that a professional engineer or geologist verify that the structural fill to be used on this project meets

<sup>2</sup> OSHA Health and Safety Standards, Final Rule, CFR 29, part 1926.



the requirements, stated below. We recommend that structural fill consist of imported sandy/gravelly soils meeting the following requirements in the table below:

**Table 2: Structural Fill Recommendations**

Sieve Size/Other	Percent Passing (by weight)
4 inches	100
3/4 inches	70 – 100
No. 4	40 – 80
No. 40	15 – 50
No. 200	0 – 20
Liquid Limit	35 maximum
Plasticity Index	15 maximum

In some situations, particles larger than 4 inches and/or more than 30 percent coarse gravel may be acceptable, but would likely make compaction more difficult and/or significantly reduce the possibility of successful compaction testing. Consequently, stricter quality control measures than normally used may be required, such as using thinner lifts and increased or full time observation of fill placement.

We recommend that utility trenches below any structural load be backfilled using structural fill. Note that most local governments and utility companies require Type A-1-a or A-1-b (AASHTO classification) soils (which overall is stricter than our recommendations for structural fill) be used as backfill above utilities in certain areas. In other areas or situations, utility trenches may be backfilled with the native soil, but the contractor should be aware that native clay and silt soils (as observed in the explorations) may be time consuming to compact due to potential difficulties in controlling the moisture content needed to obtain optimum compaction. All backfill soil should have a maximum particle size of 4 inches, a maximum Liquid Limit of 35 and a maximum Plasticity Index of 15.

If required (i.e. fill in submerged areas), we recommend that free draining granular material (clean sand and/or gravel) meet the following requirements in the table below:

**Table 3: Free-Draining Fill Recommendations**

Sieve Size/Other	Percent Passing (by weight)
3 inches	100
No. 10	0 – 25
No. 40	0 – 15
No. 200	0 – 5
Plasticity Index	Non-plastic

Three inch minus washed rock (sometimes called river rock or drain rock) and pea gravel materials usually meet these requirements and may be used as free draining fill. If free draining fill will be placed adjacent to soil containing a significant amount of sand or silt/clay, precautions should be taken to prevent the migration of fine soil into the free draining fill. Such precautions should include either placing a filter fabric between the free draining fill and the adjacent soil



material, or using a well-graded, clean filtering material approved by the geotechnical engineer.

#### **8.4 Fill Placement and Compaction**

The thickness of each lift should be appropriate for the compaction equipment that is used. We recommend a maximum lift thickness prior to compaction of 4 inches for hand operated equipment, 6 inches for most "trench compactors" and 8 inches for larger rollers, unless it can be demonstrated by in-place density tests that the required compaction can be obtained throughout a thicker lift. The full thickness of each lift of structural fill placed should be compacted to at least the following percentages of the maximum dry density, as determined by ASTM D-1557:

- In landscape and other areas not below structurally loaded areas: 90%
- Less than 5 feet of fill below structurally loaded areas: 95%
- Greater than 5 feet of fill below structurally loaded areas: 98%

Generally, placing and compacting fill at moisture contents within  $\pm 2$  percent of the optimum moisture content, as determined by ASTM D-1557, will facilitate compaction. Typically, the further the moisture content deviates from optimum the more difficult it will be to achieve the required compaction.

Fill should be tested frequently during placement and we recommend early testing to demonstrate that placement and compaction methods are achieving the required compaction. The contractor is responsible to ensure that fill materials and compaction efforts are consistent so that tested areas are representative of the entire fill.

#### **8.5 Stabilization Recommendations**

Near surface layers of clay, silt, and silty sand soils may rut and pump during grading and construction. The likelihood of rutting and/or pumping, and the depth of disturbance, is proportional to the moisture content in the soil, the load applied to the ground surface, and the frequency of the load. Consequently, rutting and pumping can be minimized by avoiding concentrated traffic, minimizing the load applied to the ground surface by using lighter equipment, partially loaded equipment, tracked equipment, by working in dry times of the year, and/or by providing a working surface for equipment.

During grading the soil in any obvious soft spots should be removed and replaced with granular material. If rutting or pumping occurs traffic should be stopped in the area of concern. The soil in rutted areas should be removed and replaced with granular material. In areas where pumping occurs the soil should either be allowed to sit until pore pressures dissipate (several hours to several days) and the soil firms up, or be removed and replaced with granular material. Typically, we recommend removal to a minimum depth of 24 inches.

For granular material, we recommend using angular well-graded gravel, such as pit run, or crushed rock with a maximum particle size of four inches. We suggest that the initial lift be approximately 12 inches thick and be compacted with a static roller-type compactor. A finer



granular material such as sand, gravelly sand, sandy gravel or road base may also be used. Materials which are more angular and coarse may require thinner lifts in order to achieve compaction. We recommend that the fines content (percent passing the No. 200 sieve) be less than 15%, the liquid limit be less than 35, and the plasticity index be less than 15.

Using a geosynthetic fabric, such as Mirafi 600X or equivalent, may also reduce the amount of material required and avoid mixing of the granular material and the subgrade. If a fabric is used, following removal of disturbed soils and water, the fabric should be placed over the bottom and up the sides of the excavation a minimum of 24 inches. The fabric should be placed in accordance with the manufacturer's recommendations, including proper overlaps. The granular material should then be placed over the fabric in compacted lifts. Again, we suggest that the initial lift be approximately 12 inches thick and be compacted with a static roller-type compactor.

## 9.0 SEISMIC AND GEOLOGIC CONSIDERATIONS

### 9.1 Seismic Design

The residential structures should be designed in accordance with the 2015 International Residential Code (IRC). The IRC designates this area as a seismic design class D<sub>1</sub>.

The site is located at approximately 40.362 degrees latitude and -111.808 degrees longitude from the approximate center of the site. The IRC site value for this property is 0.802g. The design spectral response acceleration parameters are given below.

**Table 4: Design Acceleration for Short Period**

S <sub>s</sub>	F <sub>a</sub>	Site Value (S <sub>DS</sub> )
		2/3 S <sub>s</sub> *F <sub>a</sub>
1.163g	1.035	0.802g

S<sub>s</sub> = Mapped spectral acceleration for short periods

F<sub>a</sub> = Site coefficient from Table 1613.3.3(1)

S<sub>DS</sub> = 2/3 S<sub>MS</sub> = 2/3 (F<sub>a</sub> · S<sub>s</sub>) = 5% damped design spectral response acceleration for short periods

### 9.2 Faulting

The subject property is located within the Intermountain Seismic Belt where the potential for active faulting and related earthquakes is present. Based upon published geologic maps<sup>3</sup>, no active faults traverse through or immediately adjacent to the site and the site is not located within local fault study zones. The nearest mapped fault trace is part of a group of faults beneath Utah Lake located about 1 3/4 miles south of the site.

<sup>3</sup> U.S. Geological Survey, Quaternary Fault and Fold Database of the United States, November 3, 2010



### 9.3 Liquefaction Potential

According to current liquefaction maps<sup>4</sup> for Utah County, the site is located within an area designated as "High" in liquefaction potential. Liquefaction can occur when saturated subsurface soils below groundwater lose their inter-granular strength due to an increase in soil pore water pressures during a dynamic event such as an earthquake. As part of this study, the potential for liquefaction to occur in the soils we encountered was assessed using Youd *et al*<sup>5</sup> and Boulanger & Idriss<sup>6</sup>. Potential liquefaction-induced movements were evaluated using Tokimatsu & Seed<sup>7</sup> and Youd, Hansen & Bartlett<sup>8</sup>.

Loose, saturated sands are most susceptible to liquefaction, but some loose, saturated gravels and relatively sensitive silt to low-plasticity silty clay soils can also liquefy during a seismic event. Subsurface soils were composed of sand, clay, and silt soils. Our analysis indicates that approximately up to 3½ inches of liquefaction-induced settlement and possibly up to 2½ feet of lateral spreading could occur in the vicinity of B-1 during a moderate to large earthquake event. The liquefaction potential at the site can be mitigated using one of the following alternatives:

- Connect/tie all footings together using reinforced grade beams and connect reinforced slabs to the footings so that the building will react as a cohesive unit. This may result in some tilting of the building due to differential liquefaction-induced movements. The building may also move laterally due to lateral spreading.

## 10.0 FOUNDATIONS

### 10.1 General

The foundation recommendations presented in this report are based on the soil conditions encountered during our field exploration, the results of laboratory testing of samples of the native soils, the site grading recommendations presented in this report, and the foundation loading conditions presented in Section 3.0, *Proposed Construction*, of this report. If loading conditions and assumptions related to foundations are significantly different, Earthtec should be notified so that we can re-evaluate our design parameters and estimates (higher loads may cause more settlement), and to provide additional recommendations if necessary.

<sup>4</sup> Utah Geological Survey, Liquefaction-Potential Map for a Part of Utah County, Utah, Public Information Series 28, August 1994

<sup>5</sup> Youd, T.L. (Chair), Idriss, I.M. (Co-Chair), and 20 other authors, 2001, Liquefaction Resistance of Soils: Summary Report from the 1996 NCEER and 1998 NCEER/NSF Workshops on Evaluation of Liquefaction Resistance of Soils, Journal of Geotechnical and Geoenvironmental Engineering, ASCE, October 2001, p. 817-833.

<sup>6</sup> Boulanger, R.W. and Idriss, I.M., 2006, Liquefaction Susceptibility Criteria for Silts and Clays, Journal of Geotechnical and Geoenvironmental Engineering, ASCE, November 2006, p. 1413-1426.

<sup>7</sup> Tokimatsu, K. and Seed, H.B., 1987, Evaluation of Settlements in Sands due to Earthquake Shaking, Journal of Geotechnical Engineering, ASCE, p. 861-878.

<sup>8</sup> Youd, T.L., Hansen, C.M. and Bartlett, S.F., 2002, Revised Multilinear Regression Equations for Prediction of Lateral Spread Displacement, Journal of Geotechnical and Geoenvironmental Engineering, ASCE, December 2002, p. 1007-1017.





Conventional strip and spread footings may be used to support the proposed structures after appropriate removals as outlined in Section 8.1. Foundations should not be installed on topsoil, undocumented fill, debris, combination soils, organic soils, frozen soil, or in ponded water. If foundation soils become disturbed during construction, they should be removed or compacted.

## 10.2 Strip/Spread Footings

We recommend that conventional strip and spread foundations be constructed entirely on a minimum of 24 inches of undisturbed gravel soils or on a minimum 18 inches of properly placed, compacted, and tested structural fill extending to undisturbed native soils. For foundation design we recommend the following:

- Footings founded on a minimum of 24 inches of undisturbed gravel soils may be designed using a maximum allowable bearing capacity of 2,000 pounds per square foot. Footings founded on a minimum 18 inches of structural fill may be designed using a maximum allowable bearing capacity of 2,000 pounds per square foot. The values for vertical foundation pressure can be increased by one-third for wind and seismic conditions per Section 1806.1 when used with the Alternative Basic Load Combinations found in Section 1605.3.2 of the 2015 International Building Code.
- Continuous and spot footings should be uniformly loaded and should have a minimum width of 20 and 30 inches, respectively.
- Exterior footings should be placed below frost depth which is determined by local building codes. In general, 30 inches of cover is adequate for most sites; however local code should be verified by the end design professional. Interior footings, not subject to frost (heated structures), should extend at least 18 inches below the lowest adjacent grade.
- Foundation walls and footings should be properly reinforced to resist all vertical and lateral loads and differential settlement.
- The bottom of footing excavations should be compacted with at least 4 passes of an approved non-vibratory roller prior to erection of forms or placement of structural fill to densify soils that may have been loosened during excavation and to identify soft spots. If soft areas are encountered, they should be stabilized as recommended in Section 8.5.
- Footing excavations should be observed by the geotechnical engineer prior to beginning footing construction to evaluate whether suitable bearing soils have been exposed and whether excavation bottoms are free of loose or disturbed soils.
- Because of shallow groundwater conditions encountered at the site, we anticipate that 18 inches of structural fill will be required below the proposed structure to provide a firm surface upon which to construct the proposed structure. In lieu of traditional structural fill, clean 1- to 2-inch clean gravel may be used in conjunction with a stabilization fabric, such as Mirafi 600X or equivalent, which should be placed between the native soils and the clean gravel (additional recommendations for placing clean gravel and stabilization fabric are given in Section 8.5 of this report).



- Due to shallow groundwater encountered at the site, lowest floor slab depths should be limited to 3 feet below existing site grades. This is intended to provide a minimum of 3 feet of separation between the observed groundwater condition and the bottom of the floor slab.
- Structural fill used below foundations should extend laterally a minimum of 6 inches for every 12 vertical inches of structural fill placed. For example, if 18 inches of structural fill is required to bring the excavation to footing grade, the structural fill should extend laterally a minimum of 9 inches beyond the edge of the footings on both sides.

### 10.3 Estimated Settlements

If the proposed foundations are properly designed and constructed using the parameters provided above, we estimate that total settlements should not exceed one inch and differential settlements should be one-half of the total settlement over a 25-foot length of continuous foundation, for non-earthquake conditions. Additional settlement could occur during a seismic event due to ground shaking, if more than 3 feet of grading fill is placed above the existing ground surface, if loading conditions are greater than anticipated in Section 3, and/or if foundation soils are allowed to become wetted.

### 10.4 Lateral Earth Pressures

Below grade walls act as soil retaining structures and should be designed to resist pressures induced by the backfill soils. The lateral pressures imposed on a retaining structure are dependent on the rigidity of the structure and its ability to resist rotation. Most retaining walls that can rotate or move slightly will develop an active lateral earth pressure condition. Structures that are not allowed to rotate or move laterally, such as subgrade basement walls, will develop an at-rest lateral earth pressure condition. Lateral pressures applied to structures may be computed by multiplying the vertical depth of backfill material by the appropriate equivalent fluid density. Any surcharge loads in excess of the soil weight applied to the backfill should be multiplied by the appropriate lateral pressure coefficient and added to the soil pressure. For static conditions the resultant forces are applied at about one-third the wall height (measured from bottom of wall). For seismic conditions, the resultant forces are applied at about two-third times the height of the wall both measured from the bottom of the wall. The lateral pressures presented in the table below are based on drained, horizontally placed native soils as backfill material using a 28° friction angle and a dry unit weight of 110 pcf.

**Table 5: Lateral Earth Pressures (Static and Dynamic)**

Condition	Case	Lateral Pressure Coefficient	Equivalent Fluid Pressure (pcf)
Active	Static	0.36	40
	Seismic	0.53	59
At-Rest	Static	0.53	58
	Seismic	0.73	81
Passive	Static	2.77	305
	Seismic	3.38	372

\*Seismic values combine the static and dynamic values



These pressure values do not include any surcharge, and are based on a relatively level ground surface at the top of the wall and drained conditions behind the wall. It is important that water is not allowed to build up (hydrostatic pressures) behind retaining structures. Retaining walls should incorporate drainage behind the walls as appropriate, and surface water should be directed away from the top and bottom of the walls.

Lateral loads are typically resisted by friction between the underlying soil and footing bottoms. Resistance to sliding may incorporate the friction acting along the base of foundations, which may be computed using a coefficient of friction of soils against concrete of 0.55 for native gravels or structural fill meeting the recommendations presented herein. Concrete or masonry walls shall be selected and constructed in accordance to the provision of Section R404 of the 2015 International Residential Code or sections referenced therein. Retaining wall lateral resistance design should further reference Section R404.4 for reference of Safety Factors.

The pressure and coefficient values presented above are ultimate; therefore, an appropriate factor of safety may need to be applied to these values for design purposes. The appropriate factor of safety will depend on the design condition and should be determined by the project structural engineer.

## 11.0 FLOOR SLABS AND FLATWORK

Due to shallow groundwater encountered at the site, lowest floor slab depths should be limited to 3 feet below existing site grades. This is intended to provide a minimum of 3 feet of separation between the observed groundwater condition and the bottom of the floor slab.

Concrete floor slabs and exterior flatwork may be supported on native soils after appropriate removals and grading as outlined in Section 8.1 are completed. We recommend placing a minimum 4 inches of free-draining fill material (see Section 8.3) beneath floor slabs to facilitate construction, act as a capillary break, and aid in distributing floor loads. For exterior flatwork, we recommend placing a minimum 4 inches of road-base material. Prior to placing the free-draining fill or road-base materials, the native sub-grade should be proof-rolled to identify soft spots, which should be stabilized as discussed above in Section 8.5.

For slab design, we recommend using a modulus of sub-grade reaction of 120 pounds per cubic inch. The thickness of slabs supported directly on the ground shall not be less than 3½ inches. A 6-mil polyethylene vapor retarder with joints lapped not less than 6 inches shall be placed between the ground surface and the concrete, as per Section R506 of the 2015 International Residential Code.

To help control normal shrinkage and stress cracking, we recommend that floor slabs have adequate reinforcement for the anticipated floor loads with the reinforcement continuous through interior floor joints, frequent crack control joints, and non-rigid attachment of the slabs to foundation and bearing walls. Special precautions should be taken during placement and curing of all concrete slabs and flatwork. Excessive slump (high water-cement ratios) of the concrete



and/or improper finishing and curing procedures used during hot or cold weather conditions may lead to excessive shrinkage, cracking, spalling, or curling of slabs. We recommend all concrete placement and curing operations be performed in accordance with American Concrete Institute (ACI) codes and practices.

## 12.0 DRAINAGE

### 12.1 Surface Drainage

Due to the collapse potential of native soils, wetting of subsurface soils (including those below foundations) could result in adverse settlement. Accordingly, we recommend the following:

- The contractor should take precautions to prevent significant wetting of the soil at the base of the excavation. Such precautions may include: grading to prevent runoff from entering the excavation, excavating during normally dry times of the year, covering the base of the excavation if significant rain or snow is forecast, backfill at the earliest possible date, frame floors and/or the roof at the earliest possible date, other precautions that might become evident during construction.
- Adequate compaction of foundation backfill should be provided i.e. a minimum of 90% of ASTM D-1557. Water consolidation methods should not be used.
- The ground surface should be graded to drain away from the building in all directions. We recommend a minimum fall of 10 inches in the first 10 feet.
- Roof runoff should be collected in rain gutters with down spouts designed to discharge well outside of the backfill limits, or at least 10 feet from foundations, whichever is greater.
- Sprinkler nozzles should be aimed away, and all sprinkler components kept at least 10 feet, from foundation walls. Also, sprinklers should not be placed at the top or on the face of slopes. Sprinkler systems should be designed with proper drainage and well maintained. Over-watering should be avoided.
- Any additional precautions which may become evident during construction.

### 12.2 Subsurface Drainage

Section R405.1 of the 2015 International Residential Code states, "Drains shall be provided around all concrete and masonry foundations that retain earth and enclose habitable or usable spaces located below grade." Section R310.2.3.2 of the 2015 International Residential Code states, "Window wells shall be designed for proper drainage by connecting to the building's foundation drainage system." An exception is allowed when the foundation is installed on well drained ground consisting of Group 1 soils, which include those defined by the Unified Soil Classification System as GW, GP, SW, SP, GM, and SM. The soils observed in the explorations at the depth of foundation consisted primarily of clay (CL) and silt (ML) which are



not Group 1 soils. The recommendations presented below should be followed during design and construction of the foundation drains:

- A perforated 4-inch minimum diameter pipe should be enveloped in at least 12 inches of free-draining gravel and placed adjacent to the perimeter footings. The perforations should be oriented such that they are not located on the bottom side of the pipe, as much as possible. The free-draining gravel should consist of primarily  $\frac{3}{4}$ - to 2-inch size gravel having less than 5 percent passing the No. 4 sieve, and should be wrapped with a separation fabric such as Mirafi 140N or equivalent.
- The highest point of the perforated pipe bottom should be equal to the bottom elevation of the footings. The pipe should be uniformly graded to drain to an appropriate outlet (storm drain, land drain, other gravity outlet, etc.) or to one or more sumps where water can be removed by pumping.
- A perforated 4-inch minimum diameter pipe should be installed in all window wells and connected to the foundation drain.
- To facilitate drainage beneath basement floor slabs we recommend that the minimum thickness of free-draining fill beneath the slabs be increased to at least 10 inches (approximately equal to the bottom of footing elevations). A separation fabric such as Mirafi 140N or equivalent should be placed beneath the free-draining gravel. Connections should be made to allow any water beneath the slabs to reach the perimeter foundation drain.
- The drain system should be periodically inspected and clean-outs should be installed for the foundation drain to allow occasional cleaning/purging, as needed. Proper drain operation depends on proper construction and maintenance.

### 13.0 PAVEMENT RECOMMENDATIONS

We understand that asphalt paved residential streets will be constructed as part of the project. The native soils encountered beneath the fill and topsoil during our field exploration were predominantly composed of clays. We estimate that a California Bearing Ratio (CBR) value of 3 is appropriate for these soils. Also, the near-surface native clay and silt soils are potentially collapsible, and over-excavation may be needed to minimize the potential settlement of pavements. If the fill material and topsoil is left beneath concrete flatwork and pavement areas, increased maintenance costs over time should be anticipated.

We anticipate that the traffic volume will be about 750 vehicles a day or less for the residential streets, consisting of mostly cars and pickup trucks, with a daily delivery truck and a weekly garbage truck. We anticipate that the traffic volume will be about 5,000 vehicles a day or less for the minor arterial collector, consisting of mostly cars and pickup trucks, with delivery trucks and weekly garbage trucks. Based on these traffic parameters, the design CBR given above, and the procedures and typical design inputs outlined in the UDOT Pavement Design Manual (1998), we recommend the minimum asphalt pavement section presented below.



**Table 6: Local Residential Pavement Section Recommendations**

Asphalt Thickness (in)	Compacted Roadbase Thickness (in)	Compacted Subbase Thickness (in)
3	6	12*
3	12*	0

\* Stabilization may be required

**Table 7: Minor Arterial Collector Pavement Section Recommendations**

Asphalt Thickness (in)	Compacted Roadbase Thickness (in)	Compacted Subbase Thickness (in)
3	6	20*
3	10	12*
3	14*	0

\* Stabilization may be required

If the pavement will be required to support construction traffic, more than an occasional semi-tractor or fire truck, or more traffic than listed above, our office should be notified so that we can re-evaluate the pavement section recommendations. The following also apply:

- The subgrade should be prepared by proof rolling to a firm, non-yielding surface, with any identified soft areas stabilized as discussed above in Section 8.5.
- Site grading fills below the pavements should meet structural fill composition and placement recommendations per Sections 8.3 and 8.4 herein.
- Asphaltic concrete, aggregate base and sub-base material composition should meet local, APWA or UDOT requirements.
- Aggregate base and sub-base is compacted to local, APWA, or UDOT requirements, or to at least 95 percent of maximum dry density (ASTM D 1557).
- Asphaltic concrete is compacted to local or UDOT requirements, or to at least 96 percent of the laboratory Marshall density (ASTM D 6927).

**14.0 GENERAL CONDITIONS**

The exploratory data presented in this report was collected to provide geotechnical design recommendations for this project. The explorations may not be indicative of subsurface conditions outside the study area or between points explored and thus have a limited value in depicting subsurface conditions for contractor bidding. Variations from the conditions portrayed in the explorations may occur and which may be sufficient to require modifications in the design. If during construction, conditions are different than presented in this report, Earthtec should be advised immediately so that the appropriate modifications can be made.

The findings and recommendations presented in this geotechnical report were prepared in



Geotechnical Study  
 American Fork Property  
 700 South 400 West  
 American Fork, Utah  
 Project No.: 169273

Page 17

accordance with generally accepted geotechnical engineering principles and practice in this area of Utah at this time. No warranty or representation is intended in our proposals, contracts, letters, or reports.

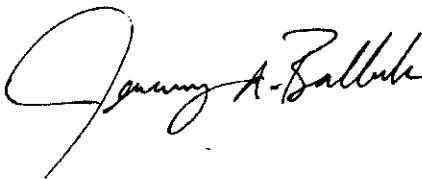
This geotechnical report is based on relatively limited subsurface explorations and laboratory testing. Subsurface conditions may differ in some locations of the site from those described herein, which may require additional analyses and possibly modified recommendations. Thus we strongly recommend consulting with Earthtec regarding any changes made during design and construction of the project from those discussed herein. Failure to consult with Earthtec regarding any such changes relieves Earthtec from any liability arising from changed conditions at the site.

To maintain continuity, Earthtec should also perform materials testing and special inspections for this project. The recommendations presented herein are based on the assumption that an adequate program of tests and observations will be followed during construction to verify compliance with our recommendations. We also assume that we will review the project plans and specifications to verify that our conclusions and recommendations are incorporated and remain appropriate (based on the actual design). Earthtec should be retained to review the final design plans and specifications so comments can be made regarding interpretation and implementation of our geotechnical recommendations in the design and specifications. Earthtec also should be retained to provide observation and testing services during grading, excavation, foundation construction, and other earth-related construction phases of the project.

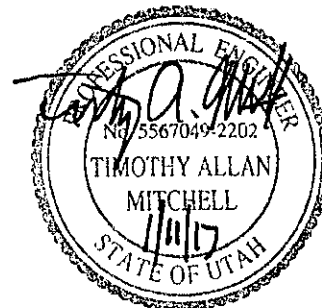
We appreciate the opportunity of providing our services on this project. If we can answer questions or be of further service, please contact Earthtec at your convenience.

Respectfully;

**EARTHTEC ENGINEERING**



Jeremy A. Balleck, E.I.T.  
 Staff Engineer



Timothy A. Mitchell, P.E.  
 Geotechnical Engineer







# AERIAL PHOTOGRAPH SHOWING LOCATION OF BORING AND TEST PITS

AMERICAN FORK PROPERTY  
700 SOUTH 400 WEST  
AMERICAN FORK, UTAH



☒ Approximate Test Pit Location



Not to Scale

PROJECT NO.: 169273



FIGURE NO.: 2

# BORING LOG

NO.: B-1

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** Great Basin  
**EQUIPMENT:** Truck Mounted Drill Rig  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 7 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** C. Allred

**AT COMPLETION  $\nabla$ :** 7 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS									
					Blows per foot	Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests	
0			TOPSOIL, silty clay with sand, moist, dark brown, roots present.											
3		GM	Silty GRAVEL with sand, medium dense (estimated), moist, brown.	X										
6		SC	Clayey SAND with gravel, very loose, moist to wet, gray.		3	24		31	10	23	41	36		
9		GM	Silty GRAVEL with sand, dense, wet, gray to brown.											
12					36									
15		SM	Silty SAND with gravel, very loose to medium dense, wet, gray.		3			44	14					
18														

**Notes:** Groundwater encountered at approximately 7 feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity/Nitrates/PH
- DS = Direct Shear
- SS = Soluble Sulfates
- UC = Unconfined Compressive Strength

LOG OF TESTHOLE TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

**PROJECT NO.:** 169273



**FIGURE NO.:** 3a

# BORING LOG

NO.: B-1

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** Great Basin  
**EQUIPMENT:** Truck Mounted Drill Rig  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 7 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** C. Allred  
**AT COMPLETION  $\nabla$ :** 7 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS								
					Blows per foot	Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests
21	[Dotted Pattern]	SM	Silty SAND with gravel, very loose to medium dense, wet, gray.	▲	11	21				33	54	13	
24													
27					24								
30	[Diagonal Hatching]	CL	Lean CLAY, medium stiff, wet, gray.	▲	6								
33													
36	[Diagonal Hatching]	SC	Clayey SAND, medium dense, wet, gray.	▲	21								
39													

LOG OF TESTHOLE TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

**Notes:** Groundwater encountered at approximately 7 feet.

**Tests Key**  
 CBR = California Bearing Ratio  
 C = Consolidation  
 R = Resistivity/Nitrates/PH  
 DS = Direct Shear  
 SS = Soluble Sulfates  
 UC = Unconfined Compressive Strength

**PROJECT NO.:** 169273



**FIGURE NO.:** 3b

# BORING LOG

NO.: B-1

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** Great Basin  
**EQUIPMENT:** Truck Mounted Drill Rig  
**DEPTH TO WATER; INITIAL  $\nabla$  :** 7 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** C. Allred

**AT COMPLETION  $\nabla$  :** 7 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS									
					Blows per foot	Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests	
42	CL	CL	Lean CLAY with sand, medium stiff to stiff, wet, gray.	10	33		39	18	0	23	77			
45														
48														
51				8										
54														
57				6										
60														

**Notes:** Groundwater encountered at approximately 7 feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity/Nitrates/PH
- DS = Direct Shear
- SS = Soluble Sulfates
- UC = Unconfined Compressive Strength

**PROJECT NO.:** 169273



**FIGURE NO.:** 3c

LOG OF TESTHOLE TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

# BORING LOG

NO.: B-1

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** Great Basin  
**EQUIPMENT:** Truck Mounted Drill Rig  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 7 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** C. Allred

**AT COMPLETION  $\nabla$ :** 7 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS								
					Blows per foot	Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests
60		CL	Lean CLAY with sand, medium stiff to stiff, wet, gray.	4									
63													
66													
69													
72			Maximum depth explored approximately 71½ feet.	9									
75													
78													

**Notes:** Groundwater encountered at approximately 7 feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity/Nitrates/PH
- DS = Direct Shear
- SS = Soluble Sulfates
- UC = Unconfined Compressive Strength

**PROJECT NO.:** 169273



**FIGURE NO.:** 3d

LOG OF TESTHOLE TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

# TEST PIT LOG

NO.: TP-1

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** JSI Excavating  
**EQUIPMENT:** Track Mounted Mini-Excavator  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 8 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** S. Howell

**AT COMPLETION  $\nabla$ :** 8 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS													
					Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests						
0																		
1			TOPSOIL, silty clay with sand, moist, dark brown, roots present.															
2			Silty CLAY with sand, stiff (estimated), moist, tan to gray.															
3		CL-ML																
4																		
5			Silty SAND, loose to medium dense (estimated), moist to wet, gray to blue gray.															
6					40	65	35	4	4	52	44							C
7			SM $\nabla$															
8																		
9																		
10																		
11			Maximum depth explored approximately 10 feet.															
12																		
13																		
14																		
15																		
16																		
17																		
18																		
19																		
20																		

**Notes:** Groundwater encountered at approximately 8 feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity
- DS = Direct Shear
- SS = Soluble Sulfates
- P = Percolation

LOG OF TESTPIT TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

**PROJECT NO.:** 169273



**FIGURE NO.:** 4

# TEST PIT LOG

## NO.: TP-2

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** JSI Excavating  
**EQUIPMENT:** Track Mounted Mini-Excavator  
**DEPTH TO WATER; INITIAL  $\nabla$  :**

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** S. Howell

**AT COMPLETION  $\nabla$  :**

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS								
					Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests	
0													
1			TOPSOIL, silty clay with sand, moist, dark brown, roots present.										
2		CL-ML	Silty CLAY, stiff (estimated), slightly moist, gray.										
3													
4		GP-GM	Poorly Graded GRAVEL with silt and sand, medium dense (estimated), moist, gray.										
5													
6		CL-ML	Sandy Silty CLAY, medium stiff (estimated), moist, gray.		25		25	4	3	44	53		
7		CL	Sandy Lean CLAY, soft to medium stiff (estimated), moist, gray to dark gray.		21	87	32	12	14	21	65	C	
8													
9													
10		SC	Clayey SAND, medium dense (estimated), moist to wet, gray.										
11													
12			Maximum depth explored approximately 11 feet.										
13													
14													
15													
16													
17													
18													
19													
20													

**Notes:** No groundwater encountered.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity
- DS = Direct Shear
- SS = Soluble Sulfates
- P = Percolation

LOG OF TESTPIT TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

**PROJECT NO.:** 169273



**FIGURE NO.:** 5

# TEST PIT LOG

## NO.: TP-3

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** JSI Excavating  
**EQUIPMENT:** Track Mounted Mini-Excavator  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 8 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** S. Howell

**AT COMPLETION  $\nabla$ :** 8 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS									
					Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests		
0														
1			TOPSOIL, silty clay with sand, moist, dark brown, roots present.											
2		GP-GM	Poorly Graded GRAVEL with silt and sand, medium dense to dense (estimated), slightly moist, gray.											
3														
4		CH	Sandy Fat CLAY, soft to medium stiff (estimated), moist, dark gray.	X										
5					34	71	50	24	8	44	48		C	
6			Clayey SAND, loose to medium dense (estimated), moist to wet, gray.											
7		SC		X										
8														
9				X										
10		CL	Lean CLAY, soft to medium stiff (estimated), wet, gray.											
11														
12			Maximum depth explored approximately 11 feet.											
13														
14														
15														
16														
17														
18														
19														
20														

**Notes:** Groundwater encountered at approximately 8 feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity
- DS = Direct Shear
- SS = Soluble Sulfates
- P = Percolation

LOG OF TESTPIT TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

**PROJECT NO.:** 169273



**FIGURE NO.:** 6



# TEST PIT LOG

## NO.: TP-4

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** JSI Excavating  
**EQUIPMENT:** Track Mounted Mini-Excavator  
**DEPTH TO WATER; INITIAL** ∇ : 8.5 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** S. Howell

**AT COMPLETION** ∇ : 8.5 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS													
					Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests						
0																		
1			TOPSOIL, silty clay with sand, moist, dark brown, roots present,															
2																		
3		SP	Poorly Graded SAND with gravel, dense (estimated), slightly moist, gray, cemented.															
4				×														
5			Sandy Lean CLAY, soft to medium stiff (estimated), moist to very moist, gray, roots present.															
6				■														
7		CL																
8																		
9			Silty GRAVEL, dense (estimated), wet, gray.	■	25	94	28	10	8	32	60							C
10		GM																
11			Maximum depth explored approximately 10½ feet.	×														
12																		
13																		
14																		
15																		
16																		
17																		
18																		
19																		
20																		

**Notes:** Groundwater encountered at approximately 8½ feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity
- DS = Direct Shear
- SS = Soluble Sulfates
- P = Percolation

LOG OF TESTPIT TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

**PROJECT NO.:** 169273



**FIGURE NO.:** 7

# TEST PIT LOG

## NO.: TP-5

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** JSI Excavating  
**EQUIPMENT:** Track Mounted Mini-Excavator  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 8 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** S. Howell

**AT COMPLETION  $\nabla$ :** 8 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS															
					Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests								
0																				
1			TOPSOIL, silty clay with sand, moist, dark brown, roots present.																	
2																				
3		CL	Lean CLAY, medium stiff (estimated), moist, gray, roots present.																	
4																				
5																				
6																				
7																				
8		GC	Poorly Graded GRAVEL with sand and clay, medium dense (estimated), moist to wet, gray.																	
9																				
10		SM	Silty SAND, medium dense (estimated), wet, gray.																	
11			Maximum depth explored approximately 10½ feet.																	
12																				
13																				
14																				
15																				
16																				
17																				
18																				
19																				
20																				

**Notes:** Groundwater encountered at approximately 8 feet.

**Tests Key**  
 CBR = California Bearing Ratio  
 C = Consolidation  
 R = Resistivity  
 DS = Direct Shear  
 SS = Soluble Sulfates  
 P = Percolation

LOG OF TESTPIT TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

# TEST PIT LOG

NO.: TP-6

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** JSI Excavating  
**EQUIPMENT:** Track Mounted Mini-Excavator  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 9 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** S. Howell

**AT COMPLETION  $\nabla$ :** 9 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS															
					Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests								
0																				
1			TOPSOIL, silty clay with sand, moist, dark brown, roots present.																	
2		CL-ML	Sandy Silty CLAY, medium stiff (estimated), moist, gray.																	
3																				
4																				
5							■	28	86	29	7	7	24	69						C
6																				
7		SM	Silty SAND, medium dense (estimated), moist, gray.																	
8																				
9							⊗													
10			Maximum depth explored approximately 9½ feet.																	
11																				
12																				
13																				
14																				
15																				
16																				
17																				
18																				
19																				
20																				

**Notes:** Groundwater encountered at approximately 9 feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity
- DS = Direct Shear
- SS = Soluble Sulfates
- P = Percolation

LOG OF TESTPIT TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

**PROJECT NO.:** 169273



**FIGURE NO.:** 9

# TEST PIT LOG

NO.: TP-7

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** JSI Excavating  
**EQUIPMENT:** Track Mounted Mini-Excavator  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 6 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** S. Howell  
**AT COMPLETION  $\nabla$ :** 6 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS									
					Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests		
0														
1			TOPSOIL, silty clay with sand, moist, dark brown, roots present.											
2		SM	Silty SAND, medium dense (estimated), slightly moist to moist, brown.											
3														
4		GP	Poorly Graded GRAVEL with silt and sand, dense (estimated), moist, gray.											
5														
6		ML	Sandy SILT with gravel, soft to medium stiff (estimated), wet, gray.											
7														
8														
9					68	51	41	9	22	24	54			C
10			Maximum depth explored approximately 9½ feet.											
11														
12														
13														
14														
15														
16														
17														
18														
19														
20														

**Notes:** Groundwater encountered at approximately 6 feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity
- DS = Direct Shear
- SS = Soluble Sulfates
- P = Percolation

PROJECT NO.: 169273



FIGURE NO.: 10

LOG OF TEST PIT TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

# TEST PIT LOG

## NO.: TP-8

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes  
**LOCATION:** See Figure No. 2  
**OPERATOR:** JSI Excavating  
**EQUIPMENT:** Track Mounted Mini-Excavator  
**DEPTH TO WATER; INITIAL  $\nabla$ :** 7 ft.

**PROJECT NO.:** 169273  
**DATE:** 12/20/16  
**ELEVATION:** Not Measured  
**LOGGED BY:** S. Howell

**AT COMPLETION  $\nabla$ :** 7 ft.

Depth (Ft.)	Graphic Log	USCS	Description	Samples	TEST RESULTS											
					Water Cont. (%)	Dry Dens. (pcf)	LL	PI	Gravel (%)	Sand (%)	Fines (%)	Other Tests				
0																
1			TOPSOIL, silty clay with sand, moist, dark brown, roots present.													
2		ML	Sandy SILT, medium stiff to stiff (estimated), slightly moist to moist, tan.													
3				█	18	65	39	8	11	31	58	C				
4																
5		GP $\nabla$	Poorly Graded GRAVEL, dense (estimated), moist to wet, gray.													
6																
7																
8																
9																
10				⊗												
11			Maximum depth explored approximately 10 feet.													
12																
13																
14																
15																
16																
17																
18																
19																
20																

**Notes:** Groundwater encountered at approximately 7 feet.

**Tests Key**

- CBR = California Bearing Ratio
- C = Consolidation
- R = Resistivity
- DS = Direct Shear
- SS = Soluble Sulfates
- P = Percolation

**PROJECT NO.:** 169273



**FIGURE NO.:** 11

LOG OF TESTPIT TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

# LEGEND

**PROJECT:** American Fork Property  
**CLIENT:** Woodside Homes

**DATE:** 12/20/16  
**LOGGED BY:** S. Howell

## UNIFIED SOIL CLASSIFICATION SYSTEM

MAJOR SOIL DIVISIONS		USCS SYMBOL		TYPICAL SOIL DESCRIPTIONS	
<b>COARSE GRAINED SOILS</b>  (More than 50% retaining on No. 200 Sieve)	<b>GRAVELS</b>  (More than 50% of coarse fraction retained on No. 4 Sieve)	CLEAN GRAVELS (Less than 5% fines)	GW	Well Graded Gravel, May Contain Sand, Very Little Fines	
		GRAVELS WITH FINES (More than 12% fines)	GP	Poorly Graded Gravel, May Contain Sand, Very Little Fines	
		<b>SANDS</b>  (50% or more of coarse fraction passes No. 4 Sieve)	CLEAN SANDS (Less than 5% fines)	SW	Well Graded Sand, May Contain Gravel, Very Little Fines
			SANDS WITH FINES (More than 12% fines)	SP	Poorly Graded Sand, May Contain Gravel, Very Little Fines
	<b>FINE GRAINED SOILS</b>  (More than 50% passing No. 200 Sieve)	<b>SILTS AND CLAYS</b>  (Liquid Limit less than 50)		CL	Lean Clay, Inorganic, May Contain Gravel and/or Sand
				ML	Silt, Inorganic, May Contain Gravel and/or Sand
			OL	Organic Silt or Clay, May Contain Gravel and/or Sand	
<b>SILTS AND CLAYS</b>  (Liquid Limit Greater than 50)			CH	Fat Clay, Inorganic, May Contain Gravel and/or Sand	
			MH	Elastic Silt, Inorganic, May Contain Gravel and/or Sand	
			OH	Organic Clay or Silt, May Contain Gravel and/or Sand	
<b>HIGHLY ORGANIC SOILS</b>			PT	Peat, Primarily Organic Matter	

### SAMPLER DESCRIPTIONS

- SPLIT SPOON SAMPLER  
(1 3/8 inch inside diameter)
- MODIFIED CALIFORNIA SAMPLER  
(2 inch outside diameter)
- SHELBY TUBE  
(3 inch outside diameter)
- BLOCK SAMPLE
- BAG/BULK SAMPLE

### WATER SYMBOLS

- Water level encountered during field exploration
- Water level encountered at completion of field exploration

- NOTES:**
1. The logs are subject to the limitations, conclusions, and recommendations in this report.
  2. Results of tests conducted on samples recovered are reported on the logs and any applicable graphs.
  3. Strata lines on the logs represent approximate boundaries only. Actual transitions may be gradual.
  4. In general, USCS symbols shown on the logs are based on visual methods only: actual designations (based on laboratory tests) may vary.

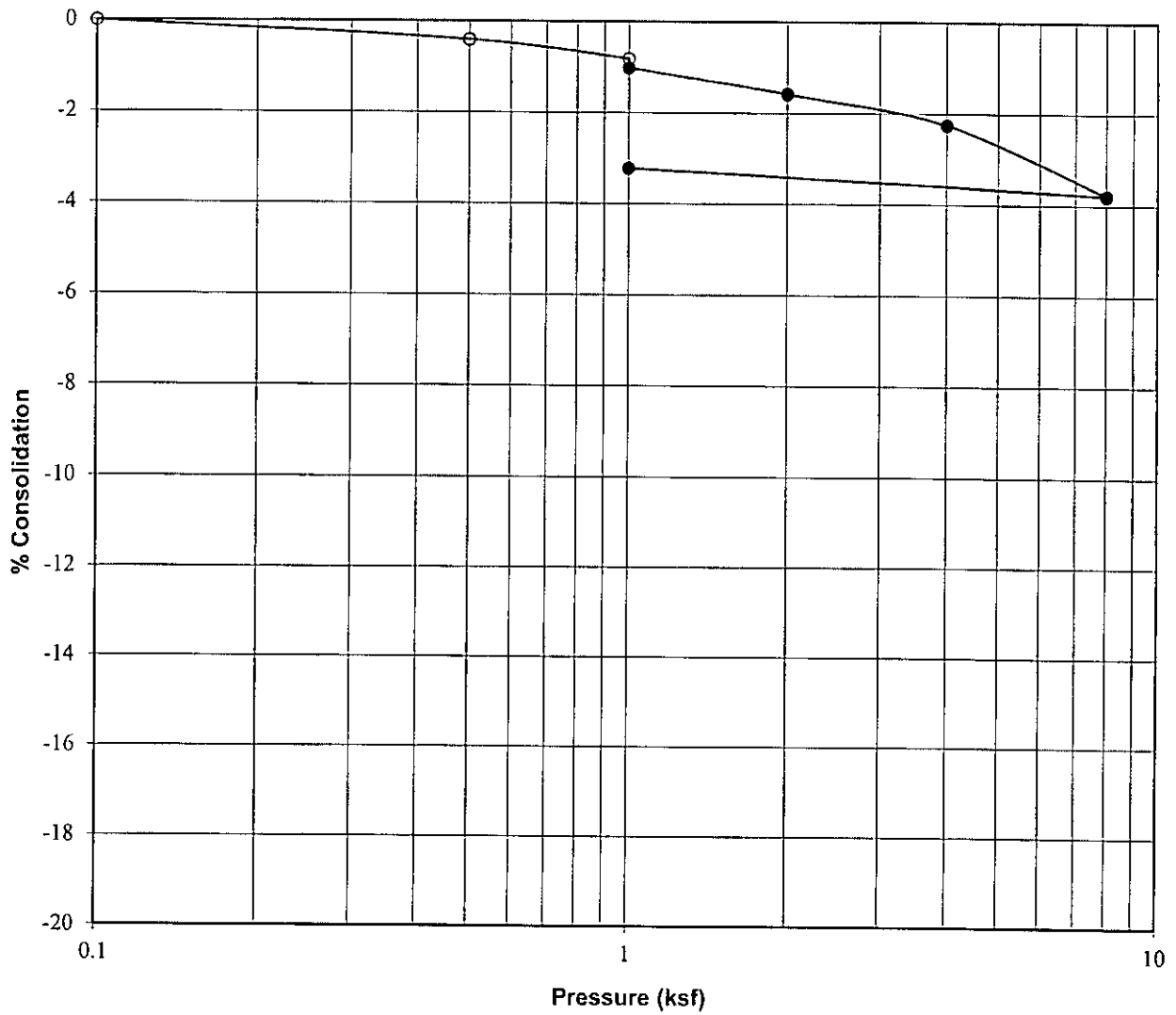
LEGEND TEST PIT LOGS.GPJ EARTHTEC.GDT 1/12/17

PROJECT NO.: 169273



FIGURE NO.: 12

# CONSOLIDATION - SWELL TEST



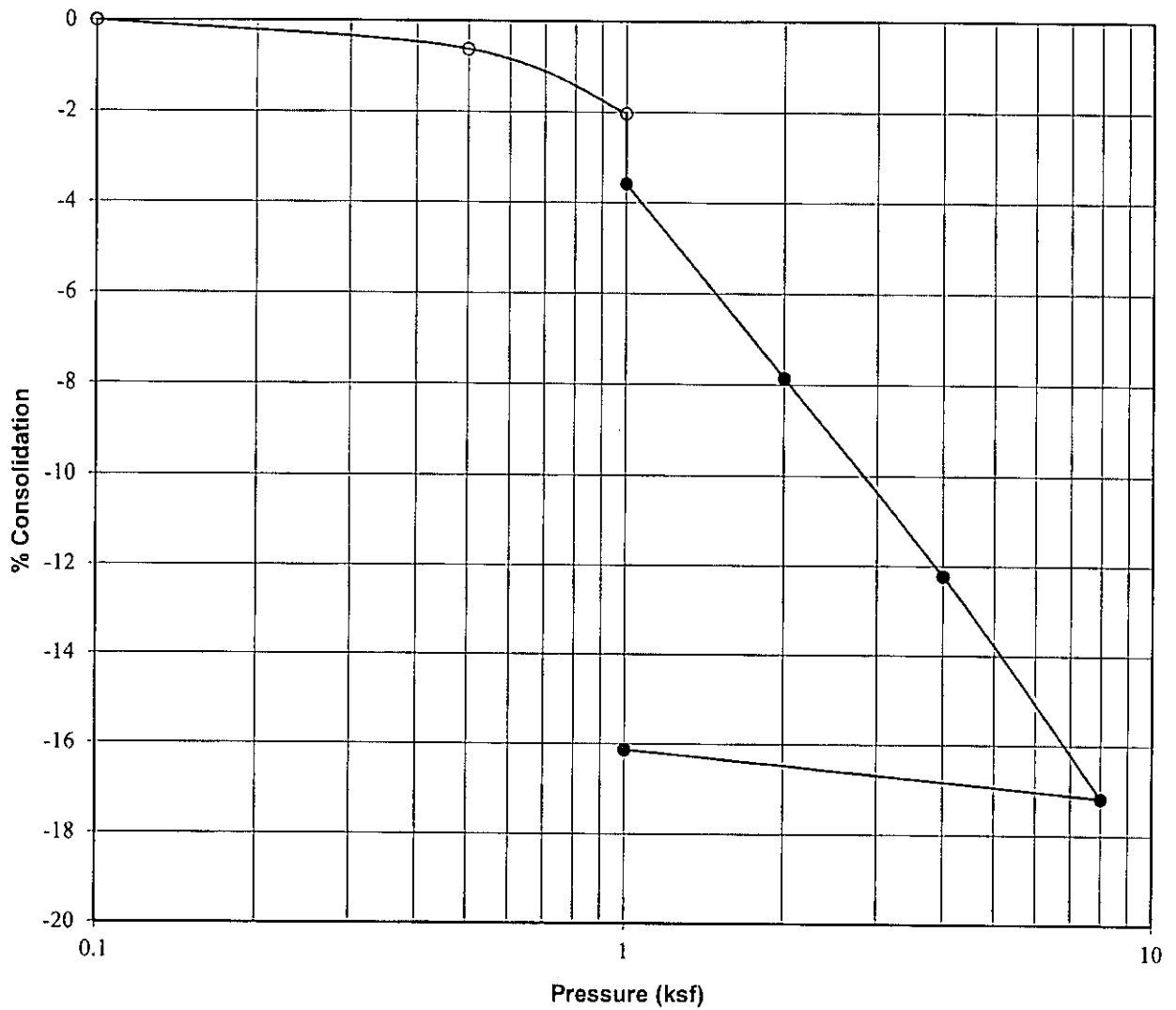
<b>Project:</b>	American Fork Property
<b>Location:</b>	TP-1
<b>Sample Depth, ft:</b>	5
<b>Description:</b>	Block
<b>Soil Type:</b>	Silty SAND (SM)
<b>Natural Moisture, %:</b>	40
<b>Dry Density, pcf:</b>	65
<b>Liquid Limit:</b>	35
<b>Plasticity Index:</b>	4
<b>Water Added at:</b>	1 ksf
<b>Percent Collapse:</b>	0.2

PROJECT NO.: 169273



FIGURE NO.: 13

# CONSOLIDATION - SWELL TEST



<b>Project:</b>	American Fork Property
<b>Location:</b>	TP-2
<b>Sample Depth, ft:</b>	6½
<b>Description:</b>	Block
<b>Soil Type:</b>	Sandy Lean CLAY (CL)
<b>Natural Moisture, %:</b>	21
<b>Dry Density, pcf:</b>	87
<b>Liquid Limit:</b>	32
<b>Plasticity Index:</b>	12
<b>Water Added at:</b>	1 ksf
<b>Percent Collapse:</b>	1.6

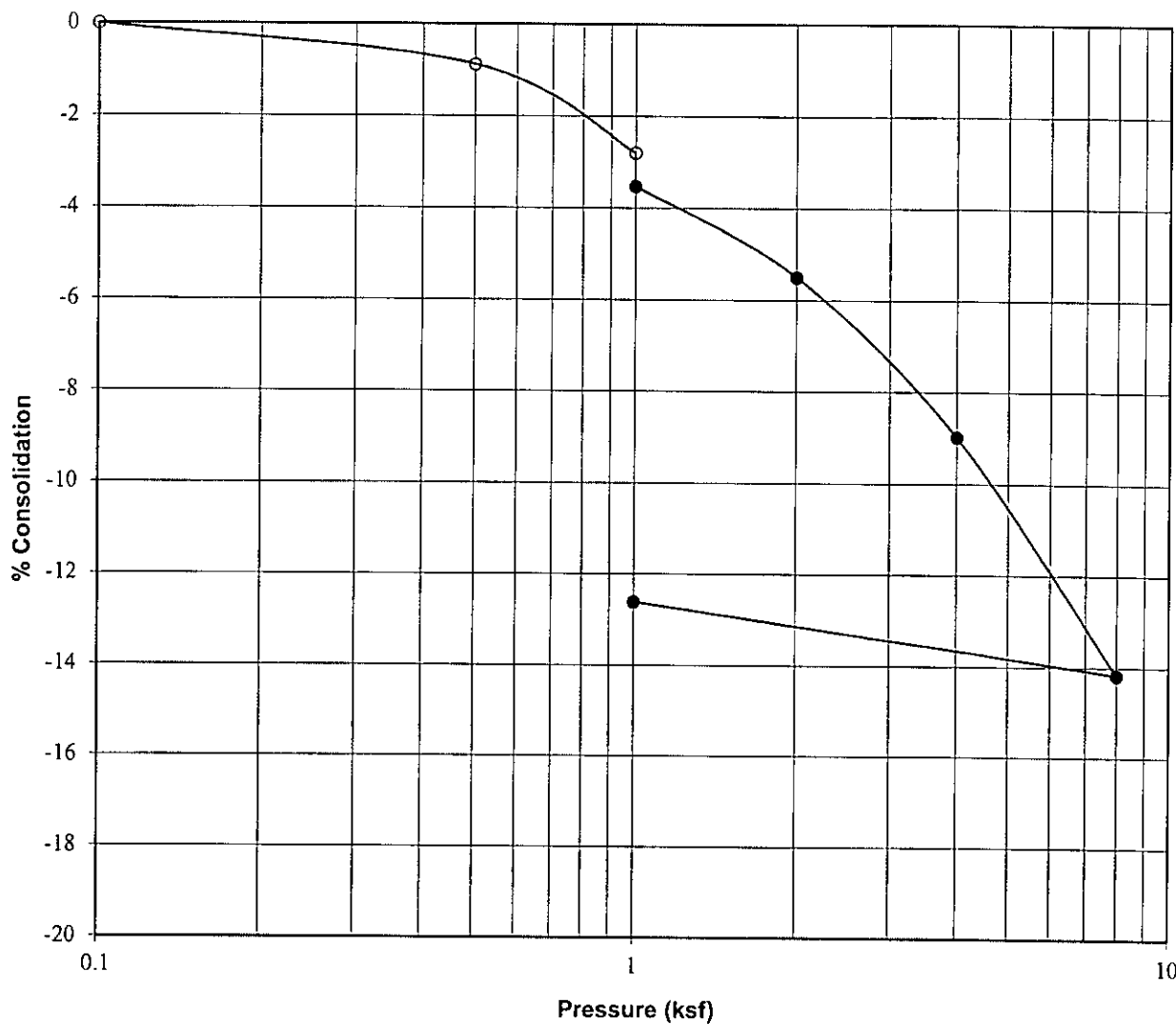
PROJECT NO.: 169273



FIGURE NO.: 14



# CONSOLIDATION - SWELL TEST



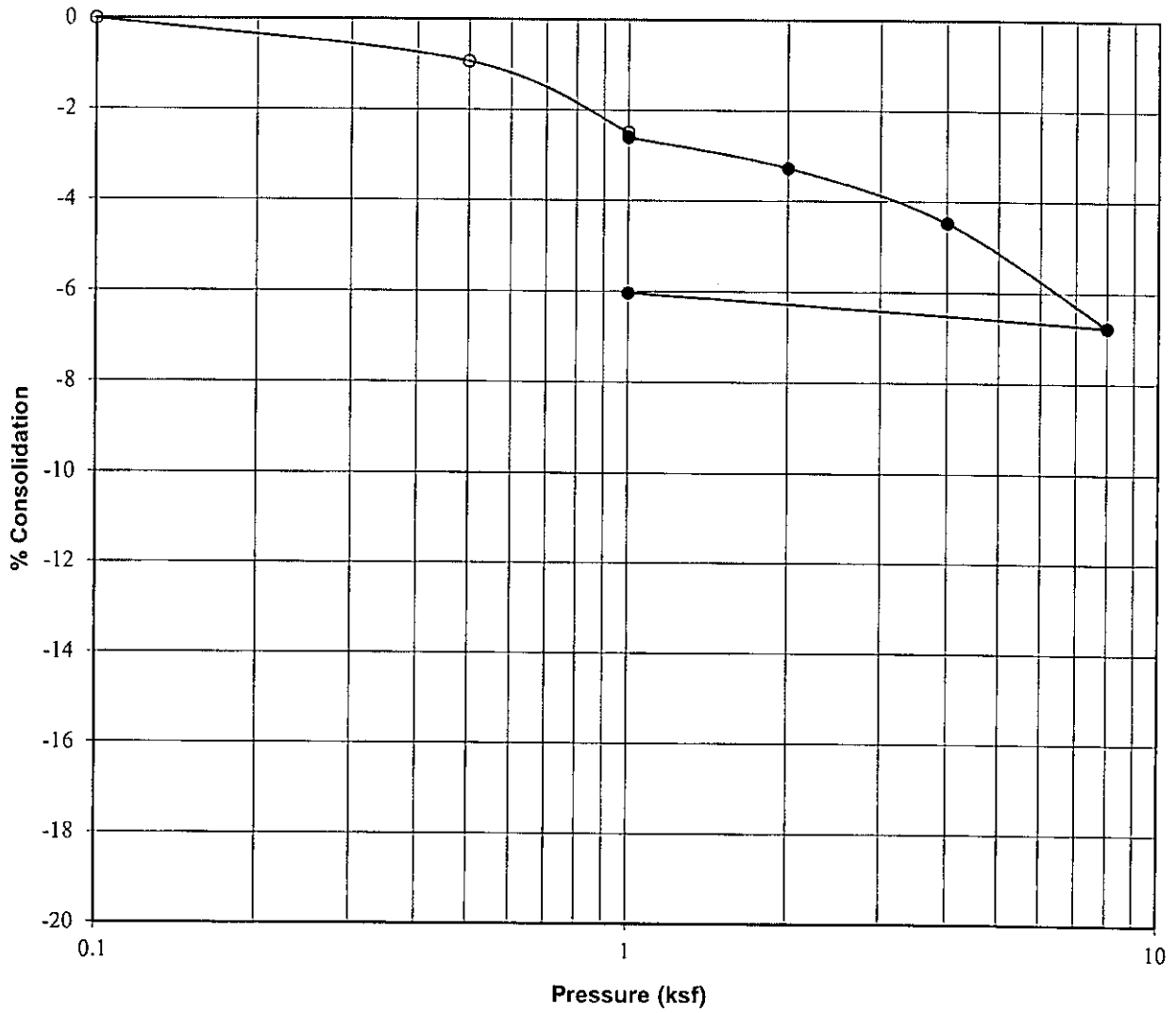
<b>Project:</b>	American Fork Property
<b>Location:</b>	TP-3
<b>Sample Depth, ft:</b>	4
<b>Description:</b>	Block
<b>Soil Type:</b>	Sandy Fat CLAY (CH)
<b>Natural Moisture, %:</b>	34
<b>Dry Density, pcf:</b>	71
<b>Liquid Limit:</b>	50
<b>Plasticity Index:</b>	24
<b>Water Added at:</b>	1 ksf
<b>Percent Collapse:</b>	0.7

PROJECT NO.: 169273



FIGURE NO.: 15

# CONSOLIDATION - SWELL TEST



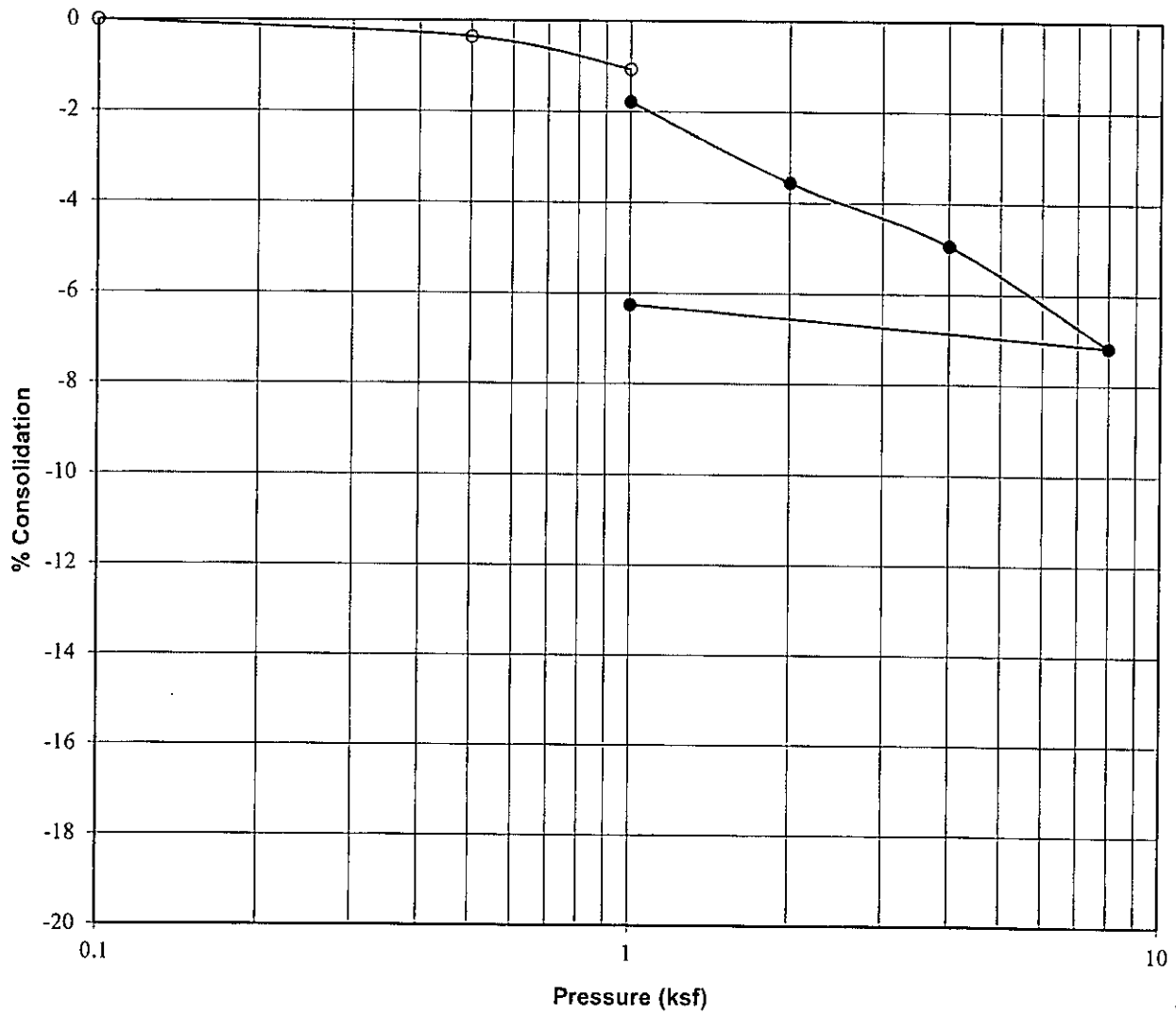
<b>Project:</b>	American Fork Property
<b>Location:</b>	TP-4
<b>Sample Depth, ft:</b>	8
<b>Description:</b>	Block
<b>Soil Type:</b>	Sandy Lean CLAY (CL)
<b>Natural Moisture, %:</b>	25
<b>Dry Density, pcf:</b>	94
<b>Liquid Limit:</b>	28
<b>Plasticity Index:</b>	10
<b>Water Added at:</b>	1 ksf
<b>Percent Collapse:</b>	0.1

PROJECT NO.: 169273



FIGURE NO.: 16

# CONSOLIDATION - SWELL TEST



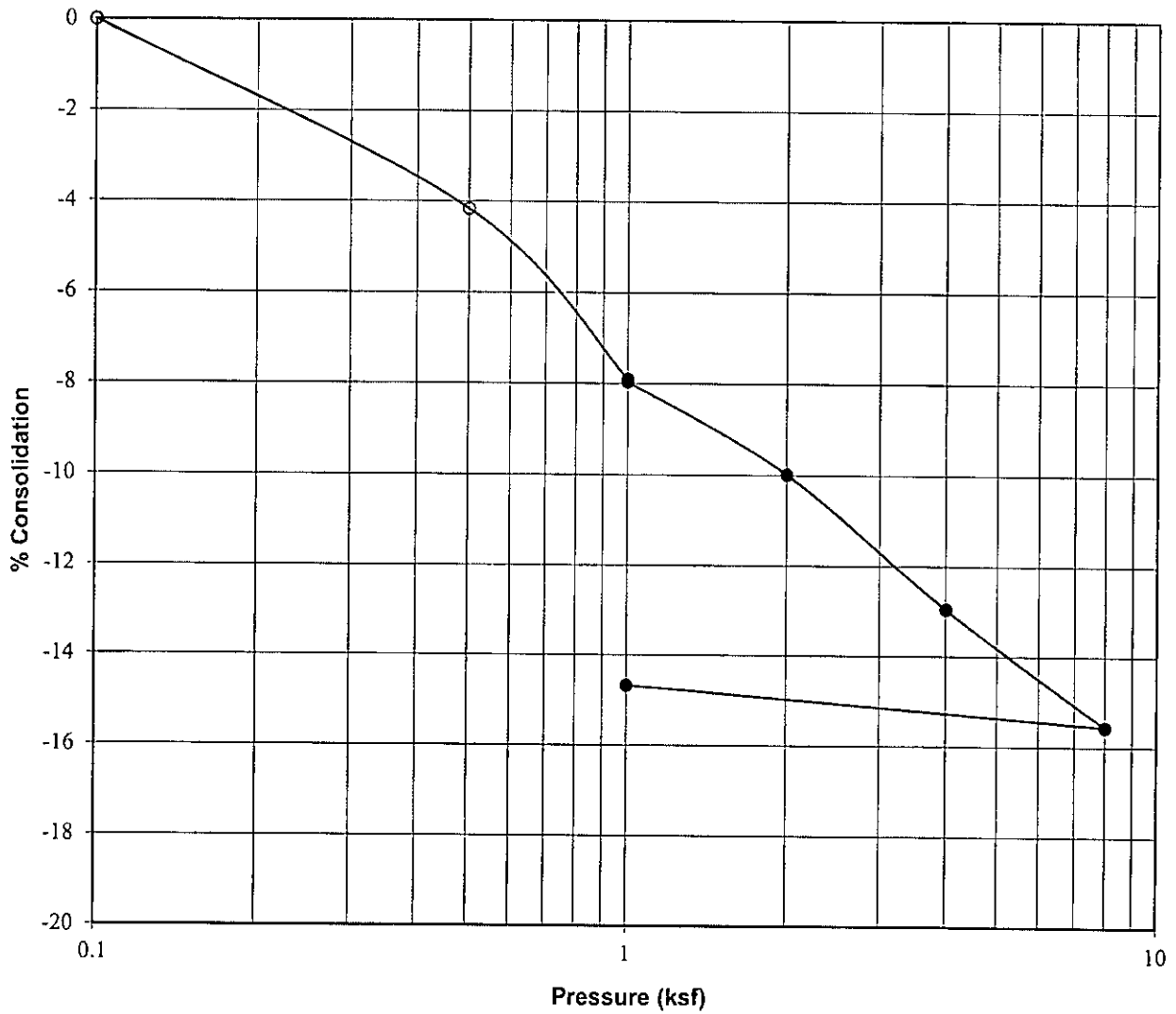
<b>Project:</b>	American Fork Property
<b>Location:</b>	TP-6
<b>Sample Depth, ft:</b>	4
<b>Description:</b>	Block
<b>Soil Type:</b>	Sandy Silty CLAY (CL-ML)
<b>Natural Moisture, %:</b>	28
<b>Dry Density, pcf:</b>	86
<b>Liquid Limit:</b>	29
<b>Plasticity Index:</b>	7
<b>Water Added at:</b>	1 ksf
<b>Percent Collapse:</b>	0.7

PROJECT NO.: 169273



FIGURE NO.: 17

# CONSOLIDATION - SWELL TEST



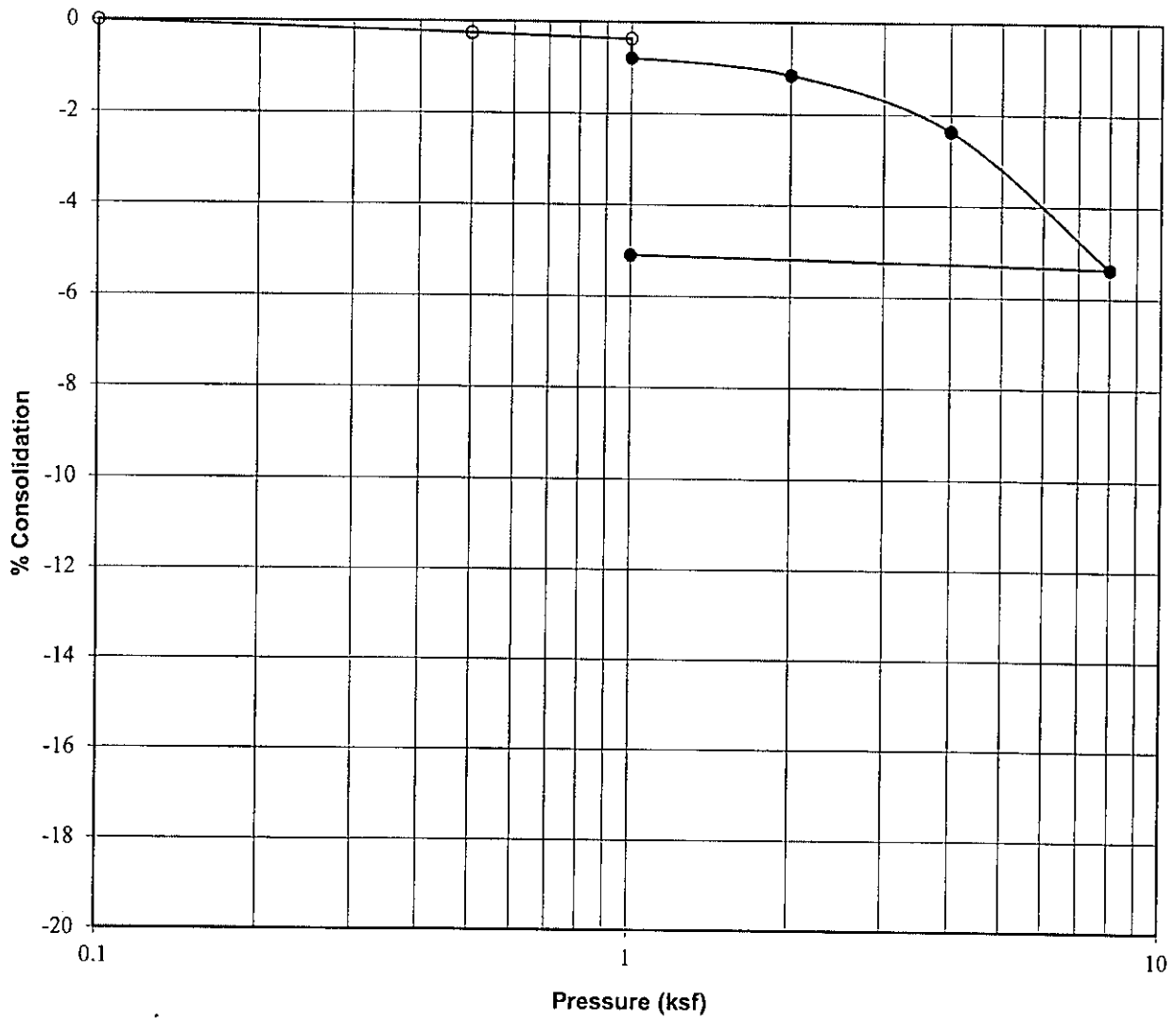
<b>Project:</b>	American Fork Property
<b>Location:</b>	TP-7
<b>Sample Depth, ft:</b>	8
<b>Description:</b>	Block
<b>Soil Type:</b>	Sandy SILT with gravel (ML)
<b>Natural Moisture, %:</b>	68
<b>Dry Density, pcf:</b>	51
<b>Liquid Limit:</b>	41
<b>Plasticity Index:</b>	9
<b>Water Added at:</b>	1 ksf
<b>Percent Collapse:</b>	0.1

PROJECT NO.: 169273



FIGURE NO.: 18

# CONSOLIDATION - SWELL TEST

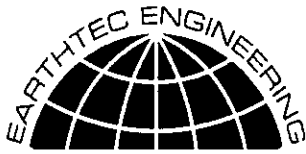


<b>Project:</b>	American Fork Property
<b>Location:</b>	TP-8
<b>Sample Depth, ft:</b>	2½
<b>Description:</b>	Block
<b>Soil Type:</b>	Sandy SILT (ML)
<b>Natural Moisture, %:</b>	18
<b>Dry Density, pcf:</b>	65
<b>Liquid Limit:</b>	39
<b>Plasticity Index:</b>	8
<b>Water Added at:</b>	1 ksf
<b>Percent Collapse:</b>	0.4

PROJECT NO.: 169273



FIGURE NO.: 19



1497 West 40 South  
Lindon, Utah - 84042  
Phone (801) 225-5711

840 West 1700 South, #10  
Salt Lake City, Utah - 84104  
Phone (801) 787-9138

1596 W. 2650 S. #108  
Ogden, Utah - 84401  
Phone (801) 399-9516

January 17, 2019

Woodside Homes  
460 West 50 North, Suite 200  
Salt Lake City, UT 84101

**Re: Pavement Addendum  
Stonecreek C  
700 South  
American Fork, Utah  
Job No: 169273**

Gentlemen:

This letter is an addendum to the geotechnical report<sup>1</sup> that was completed by Earthtec Engineering. This addendum was requested to provide pavement sections with 4 inches of asphalt for the roadways of the minor arterial collectors.

### **Pavement Recommendations**

We understand that asphalt paved residential streets will be constructed as part of the project, and a minimum of 4 inches of asphalt is required for the Minor Arterial Collectors Roadways. The native soils encountered beneath the fill and topsoil during our field exploration were predominantly composed of clays. We estimate that a California Bearing Ratio (CBR) value of 3 is appropriate for these soils.

We anticipate that the traffic volume will be about 5,000 vehicles a day or less for the minor arterial collector, consisting of mostly cars and pickup trucks, with delivery trucks and weekly garbage trucks. Based on these traffic parameters, the design CBR given above, and the procedures and typical design inputs outlined in the UDOT Pavement Design Manual (2008), we recommend the minimum asphalt pavement section presented below.

#### **Minor Arterial Collector Pavement Section Recommendations**

Asphalt Thickness (in)	Compacted Roadbase Thickness (in)	Compacted Subbase Thickness (in)
4	8	12*
4	6	16*

\* Stabilization may be required

If the pavement will be required to support construction traffic, more than an occasional semi-tractor or fire truck, or more traffic than listed above, our office should be notified so that we can re-evaluate the pavement section recommendations. All other recommendations in the referenced report should be followed.

### **General Conditions**

The same conditions of the geotechnical report apply to this addendum. The recommendations

<sup>1</sup> Geotechnical Study, American Fork Property, 700 South 400 West, American Fork, Utah, Project No. 169273, January 11, 2017



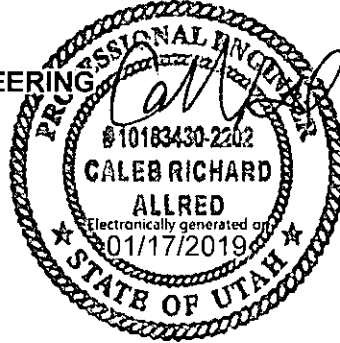
Pavement Addendum  
Stonecreek C  
700 South  
American Fork, Utah  
Job No: 169273

presented in this letter were conducted within the limits prescribed by our client, with the usual thoroughness and competence of the engineering profession in this area at this time. No warranty or representation is intended in our proposals, contracts, reports, or letters.

**Closure**

We appreciate the opportunity of providing our services on this project. If we can answer questions or be of further service, please call.

Respectfully,  
EARTHTEC ENGINEERING



Caleb R. Allred, P.E.  
Project Engineer

Timothy A. Mitchell, P.E.  
Senior Geotechnical Engineer





1497 West 40 South  
 Lindon, Utah - 84042  
 Phone (801) 225-5711

840 West 1700 South, #10  
 Salt Lake City, Utah - 84104  
 Phone (801) 787-9138

1596 W. 2650 S. #108  
 Ogden, Utah - 84401  
 Phone (801) 399-9516

June 6, 2019

Woodside Homes  
 460 West 50 North, Suite 200  
 Salt Lake City, UT 84101

**Re: Pavement Addendum 2  
 Stonecreek C  
 700 South  
 American Fork, Utah  
 Job No: 169273**

Gentlemen:

This letter is an addendum to the geotechnical report<sup>1</sup> that was completed by Earthtec Engineering. This addendum was requested to provide pavement section for 700 South American Fork has 700 North classified as a collector and the number of trucks is typically at least 4% of the annual average daily traffic (AADT). The pavement section recommended by Earthtec Engineering in Addendum 1 is only 3% of the AADT. This Addendum is to provide a pavement section meeting the city recommendations.

#### **Pavement Recommendations**

We understand that asphalt paved residential streets will be constructed as part of the project, and a minimum of 4 inches of asphalt is required for the Minor Arterial Collectors Roadways. The native soils encountered beneath the fill and topsoil during our field exploration were predominantly composed of clays. We estimate that a California Bearing Ratio (CBR) value of 3 is appropriate for these soils.

We anticipate that the traffic volume will be about 5,000 vehicles a day or less for the minor arterial collector, consisting of mostly cars and pickup trucks, with delivery trucks and weekly garbage trucks, and 4 percent of the AADT are trucks larger than a pickup truck or small utility truck. Based on these traffic parameters, the design CBR given above, and the procedures and typical design inputs outlined in the UDOT Pavement Design Manual (2008), we recommend the minimum asphalt pavement section presented below.

#### **Minor Arterial Collector Pavement Section Recommendations**

Asphalt Thickness (in)	Compacted Roadbase Thickness (in)	Compacted Subbase Thickness (in)
4½	8	12*
4	10	12*

\* Stabilization may be required

If the pavement will be required to support construction traffic, more than an occasional semi-tractor or fire truck, or more traffic than listed above, our office should be notified so that we can re-evaluate the pavement section recommendations. All other recommendations in the

<sup>1</sup> Geotechnical Study, American Fork Property, 700 South 400 West, American Fork, Utah, Project No. 169273, January 11, 2017





Pavement Addendum 2  
Stonecreek C  
700 South  
American Fork, Utah  
Job No: 169273

Page 2

referenced report should be followed.

### General Conditions

The same conditions of the geotechnical report apply to this addendum. The recommendations presented in this letter were conducted within the limits prescribed by our client, with the usual thoroughness and competence of the engineering profession in this area at this time. No warranty or representation is intended in our proposals, contracts, reports, or letters.

### Closure

We appreciate the opportunity of providing our services on this project. If we can answer questions or be of further service, please call.

Respectfully;

**EARTHTEC ENGINEERING**

Caleb R. Allred, P.E.  
Project Engineer

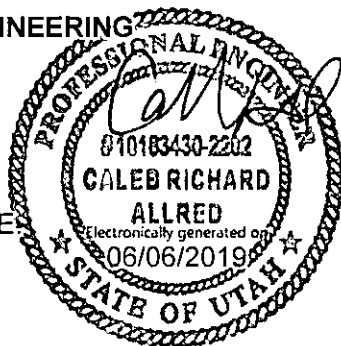
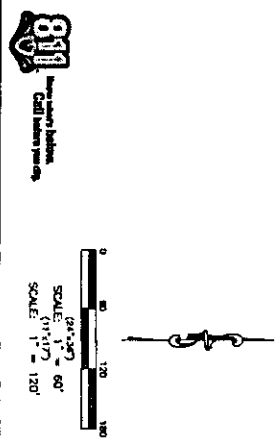


EXHIBIT C

- GENERAL NOTES**
1. ALL CONSTRUCTION TO BE DONE ACCORDING TO THE AMERICAN PAPER CITY
  2. BEFORE CONSTRUCTION, AN EROSION & SEDIMENTATION CONTROL PLAN SHALL BE SUBMITTED TO THE CITY ENGINEER FOR REVIEW AND APPROVAL.
  3. ALL CONSTRUCTION SHALL BE DONE WITHIN THE SPECIFIED TIME FRAME.
  4. ALL CONSTRUCTION SHALL BE DONE WITHIN THE SPECIFIED TIME FRAME.
  5. ALL CONSTRUCTION SHALL BE DONE WITHIN THE SPECIFIED TIME FRAME.
  6. ALL CONSTRUCTION SHALL BE DONE WITHIN THE SPECIFIED TIME FRAME.
  7. ALL CONSTRUCTION SHALL BE DONE WITHIN THE SPECIFIED TIME FRAME.
  8. ALL CONSTRUCTION SHALL BE DONE WITHIN THE SPECIFIED TIME FRAME.
  9. ALL CONSTRUCTION SHALL BE DONE WITHIN THE SPECIFIED TIME FRAME.
  10. ALL CONSTRUCTION SHALL BE DONE WITHIN THE SPECIFIED TIME FRAME.

- 1. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 2. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 3. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 4. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 5. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 6. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 7. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 8. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 9. 12" CONC. 12" OF 20# REIN. 12" DIA.
- 10. 12" CONC. 12" OF 20# REIN. 12" DIA.



NO.	DATE	BY	REVISION
1	10/15/19	TRANE	ISSUED FOR PERMIT
2	10/15/19	TRANE	REVISED PER CITY COMMENTS
3	10/15/19	TRANE	REVISED PER CITY COMMENTS

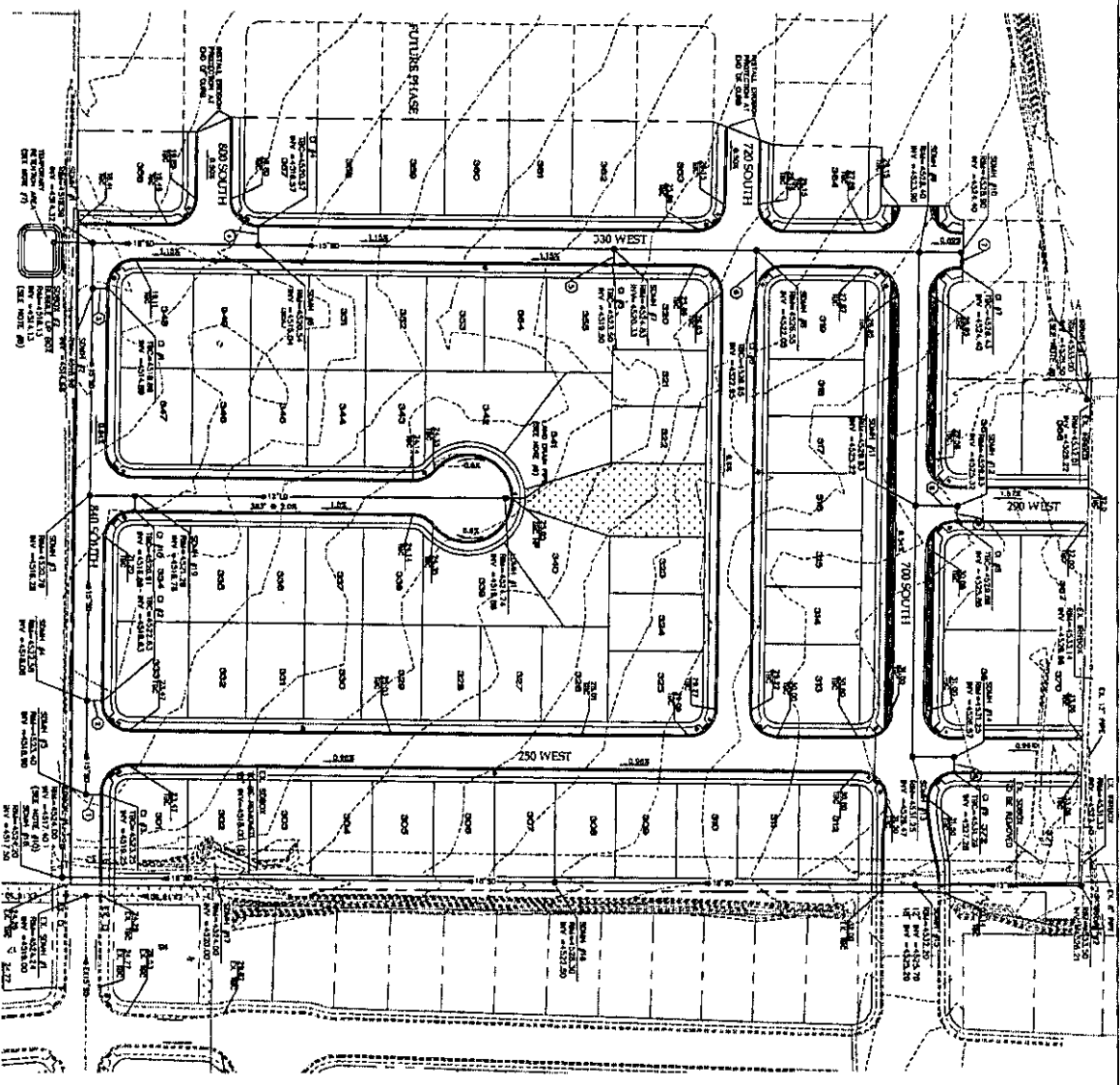
**TRANE ENGINEERING, P.C.**  
 CONSULTING ENGINEERS AND LAND SURVEYORS  
 27 EAST MAIN LEHI, UTAH 84043 (801) 788-4444

AMERICAN FORK, UTAH

**STONECREEK PLAT "C"**  
 A RESIDENTIAL SUBDIVISION

GRADING AND DRAINAGE

JOB NO. 19-04  
 SHEET NO. 3



AMERICAN FORK CITY  
 PUBLIC WORKS DEPARTMENT

AUG 22 2019

APPROVED FOR CONSTRUCTION

